

Classification

D

CURRENT PROCESS AND PLANT DATA TECHNICAL SPECIFICATIONS N2O

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| 1 | General plant information | |
|-------|---|--|
| 1.1 | Plant type (Dual Pressure/Mono-High/Mono-Medium/Mono- Low) | Mono-High |
| 1.2 | Reactor supplier (Grande Paroisse , Uhde , Wetherley , other) | Girdler |
| 1.3 | Year of start-up | First commissioning in the 1960s (Canada) and new commissioning and EMP in mid-2018 (Argentina). |
| 1.4 | Number of reactors | 1 |
| 1.5 | Reactor pressure (bar, abs) | 10 |
| 1.6a | Reactor internal diameter in mm (basket) (10-E-151) | 756 mm (Circular) |
| 1.6a | Reactor internal diameter in mm (basket) (10-R-201) | 831,85 mm (Circular) |
| 1.7 | Gauze temperature (°C) (With new gauze) | 910°C |
| 1.8 | Production rate, design (100% Metric Tons HNO ₃ /day) | 180 |
| 1.9 | Production rate, real (100% Metric Tons HNO ₃ /day) | 170 |
| 1.10 | HNO ₃ concentration in the final product (%) | 56 |
| 1.11 | Normal duration of the productive campaign (months) | 3 |
| 1.12 | Operation time (days per year) | 330 |
| 1.13a | Ammonia flow to reactor (kg/h) | 2.221 |
| 1.13b | Ammonia flow to reactor (Nm3/h) | 2.892 |
| 1.14a | Primary air flow to ammonia reactor (kg /h) | 33.168 |
| 1.14b | Primary air flow to ammonia reactor (Nm³/h) | 25.711 |
| 1.15a | Secondary air flow (kg /h) | 4.495 |
| 1.15b | Secondary air flow (Nm³/h) | 3.333 |
| 1.16 | Temperature of the gas mixture (air/NH ₃) to the reactor (°C) | 240 |
| 1.17 | Conversion efficiency of the plant at the beginning of the campaign (% or kgNH $_3$ /teHNO $_3$) | 0.99 |
| 1.18 | Plant conversion efficiency at the end of the campaign (%) | 88-91 |
| 2 | Pt gauze per reactor | |
| 2.1 | Material (Pt% / Rh%) | 95/5 |
| 2.2 | Diameter (mm) | 831,85 mm (Circular) |
| 2.3 | Number of gauze | Cant: 13 X 3 |
| 2.4 | Gauze supplier | Hereaus |
| 3 | Change of Pt gauze per reactor | |
| 3.1 | Average number of stops per campaign in the last three campaigns | 2 (one scheduled for mesh change and one unplanned stoppage) |



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| 3.2 | Number of stops that were not planned | 1 |
|-------|---|---|
| 3.3 | Date of next scheduled stoppage | Approx.Every 3 months for a mesh change and a general shutdown plant |
| 3.4 | Planned changes to the composition of Pt gauze in the future? | NO |
| 4 | Reactor Basket / Pressure Drop Data | |
| 4.1 | Type of support system installed (basket with Raschig rings , others) | Mesh: Nickel / Chrome |
| 4.2 | Support system depth (mm) | 142,87mm |
| 4.3 | Available depth for a secondary catalyst under gauze (mm) | 242,89mmDistance between the mesh and the top of the exchanger tubes |
| 5 | NSCR and tail gas information | |
| 5.1 | NOx abatement unit installed (Yes / No) | Yes |
| 5.2 | NOx abatement unit | Before expand(between boilers 10-BO-155/156) |
| 5.3 | NOx reduction system type (SCR /NSCR) | NSCR |
| 5.4 | NSCR catalyst (precious metal, base metal, zeolite) | Pt-Rh-Pd Impregnating in ceramic base |
| 5.5 | NSCR Catalyst Supplier | ECS |
| 5.6 | Maximum temperature allowed in the NSCR reactor (°C) | 732 |
| 5.7 | NSCR catalyst age (years) | Lifespan: 3-4 years Last upload: April 2023 |
| 5.8 | NOx regulation limit (ppm) | 50 |
| 5.9 | NOx content before the reactor (ppm) | 5,500 |
| 5.10 | NOx content after reactor (ppm) | < 50 |
| 5.11a | Gas flow before NSCR (kg/h /h) | 29.348 |
| 5.11b | Gas flow before NSCR (Nm 3 / h) | 23.243 |
| 5.12a | Gas flow after NSCR (kg/h /h) | 29.518 |
| 5.12b | Gas flow after NSCR (Nm ³ /h) | 23.083 |
| 5.13 | Tail gas temperature at the outlet of the absorption tower (°C) | 28-34 |
| 5.14 | Tail gas temperature (°C) before NSCR | 470 - 485 |
| 5.15 | Tail gas temperature (°C) after NSCR | 710 - 730 |
| 5.16 | NSCR O2 content (% vol.) | 1.3 – 1.5% (up to 2.5% could be achieved but due to the requirements of the current abatement |



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| | | system it operates between 1.3-1.5%) |
|------|--|---|
| 5.17 | Tail gas temperature (°C) before expander | 590 - 610 |
| 5.18 | Tail gas temperature (°C) before expander (max. Allowable) | 640 |
| 5.19 | Tail gas temperature (°C) after turbine | 240 - 270 |
| 5.20 | Tail gas pressure at the outlet of the absorption tower (bar a) | 7.7-8.2 |
| 5.21 | Tail gas pressure at the absorption tower inlet (bar a) | 8.7-9.2 |
| 5.22 | Tail gas pressure (bar a) before turbine | 7.5-8.0 |
| 5.23 | Tail gas pressure (bar absolute) after turbine | ~1 |
| | Reducing agents for NSCR: | |
| 5.24 | Ammonia Plant Purge Gas Flow (kg/h) Natural Gas flow | 360 kg/h 200 kg/h |
| 5.25 | Purge gas compositionNatural Gas Composition | 30 % CH4; 7 % H2; 26 % Ar; 37% N291% CH4 – 5,5% C2H6– 0,5% C3H8 – 0,2% C4H10 – 2,8% otros |
| 6 | Chimney information | |
| 6.2 | Distance from chimney to control room (m) | 100 aprox |
| 6.3 | Distance from sampling location (possible/existing) at chimney to ground level | 30 |
| 6.4 | Sampling platform required (Yes/No) | No |
| 6.5 | Access to the sampling platform (stairs) | Through stairs |
| 6.6 | O ₂ content in tail gases (% vol.) | 0% |
| 6.7 | Maximum allowable additional pressure drop caused by the tertiary reduction system | 0.2 kg/cm2g |
| 7 | Steam generation with NSCR heat exchanger The pre- and post-NSCR boilers are considered. | |
| 7.1 | Steam flow generated (kg/h) | 2650 |
| 7.2 | Generated steam temperature (°C) | 230 |
| | Generated steam pressure (bar) | 15 – 15,5 |
| 7.3 | Generated steam pressure (bar) | 10 – 10,0 |

| Austin Powder |
|---------------|
| Argentina SA |
| Petrochemical |
| Division |

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